10/500981
DT Rec'd PCT/PTO 02 JUL 2004

POLARIZATION DIVERSITY DETECTION USING A POLARIZATION MULTIPLEXED LOCAL OSCILLATOR

BACKGROUND OF THE INVENTION

The present invention relates to determination of an optical property of an optical device under test, in particular to optical polarization diversity detection.

SUMMARY OF THE INVENTION

It is an object of the invention to provide improved optical polarization diversity detection.

The object is solved by the independent claims.

The prior art measuring concept according to EP 1113250 acquired the Jones matrix elements of a DUT by using a laser signal which was swept in wavelength as stimulus. The output signal was analyzed by a coherent superposition with a LO signal. To provide polarization resolved measurement the output signal was split into two orthogonal components each of which were superimposed with the LO signal. To unambiguously acquire all 4 elements of the Jones matrix it was necessary to perform this measurement with two input polarization states. Therefore it was either necessary to perform an extra wavelength sweep or to insert a PDU into the DUT path allowing to stimulate the DUT with two polarization states 'simultaneously' according to US 09/941133.

In an embodiment of the present invention it is proposed to insert a PDU according to US 09/941133, the disclosure of which is incorporated herein by reference, into the LO path (PDU_{LO}) so that two orthogonal polarization states, a first state of polarization (SOP_H) and a second state of polarization (SOP_V), occur at the output of the PDU_{LO}. The two orthogonal components have traveled different optical paths inside the PDU and thus produce interference signatures at different electrical frequencies (f_H and f_V) when combined with the DUT signal at the detector.

Therefore, in an embodiment of the present invention it is disclosed an

enhancement of the interferometric measurement method of EP 1113250, the disclosure of which is incorporated herein by reference, which is able to measure the chromatic dispersion (CD) and polarization mode dispersion (PMD) of a device under test (DUT) with high accuracy. According to an embodiment of the present invention the use of a polarization delay unit (PDU) according to US 09/941133 in the local-oscillator (LO) path of the DUT interferometer allows to replace the polarization diversity detector (PDR) by a single detector to reduce complexity of the detection scheme. In this way, problems associated with detector symmetry and extinction ratio of the polarization beam splitter (PBS) can be solved since there is only one detector left so that the PBS can be omitted.

The interference signatures created by the interference of the DUT signal with SOP_H and SOP_V respectively can be distinguished preferably by applying band pass filters of appropriate center frequency and bandwidth.

Furthermore, amplitude and phase of the two spectral components only depend on the fraction of the DUT signal having the same polarization as the interfering LO signal. That is, the DUT signal is inherently decomposed into two polarizations SOP_H and SOP_V interfering with the corresponding two LO signals and producing signatures at f_H and f_V respectively. In an embodiment of the present invention the AC part of the detector signal can be written as follows:

$$P_{AC}(\omega) = E_{LO} E_{DUT} \left(\overrightarrow{sop}_{DUT} \cdot \overrightarrow{sop}_H \right) \cos\left(\varphi_H + \underbrace{\left(\tau_{DUT} - \tau_{LO,H} \right)}_{f_H} \omega \right) +$$
$$E_{LO} E_{DUT} \left(\overrightarrow{sop}_{DUT} \cdot \overrightarrow{sop}_V \right) \cos\left(\varphi_V + \underbrace{\left(\tau_{DUT} - \tau_{LO,V} \right)}_{f_V} \omega \right)$$

Hence, the polarization dependence of the interference effect can be used to realize polarization diversity detection and the information contained in the two signatures is equivalent to a prior art PDR output according to EP 1113250.

To produce a signal which can be processed in the established way by the Jones matrix eigenanalysis, the two spectral components can be separated using two bandpass filters (possibly FIR filters). Then the faster oscillating

signal can be shifted in frequency so that it is aligned to the slower oscillating signal. This can easily be achieved if the differential group delay (DGD) of the PDU ($DGD_{PDU} = \tau_{LO,H}-\tau_{LO,V}$) is known. Then a linear phase term can be subtracted from the analytical signal by multiplying with $\exp(-(\tau_{LO,H}-\tau_{LO,V})\omega)$. Now the two generated signals are identical to those which would have been generated by a coherent prior art PDR detector.

Furthermore, the prior art concepts incorporating PDRs as detectors suffered from the fact that it is very difficult to choose an optimum LO polarization at more than two PDRs simultaneously. This problem can be solved by an embodiment of the present invention since the polarization of the LO signal does not enter the evaluation anymore. This property makes this embodiment particularly well suited for multiport device characterization where the LO is distributed among several detectors.

Using the prior art concept according to EP 1113250 for multiport device characterization requires distributing the LO signal among several PDR detectors. Unfortunately it is very difficult to provide an optimum input polarization of the LO signal at every PDR simultaneously simply by adjusting the input polarization of the whole setup. Therefore, with the cited prior art multiport devices can only be measured by performing several sweeps and adjusting the optimum input polarization for each sweep. Another solution would be to insert a one dimensional polarization controller (i.e. a wave plate of tunable retardation) in front of each PDR. This gives the opportunity to acquire all data in a single or at least in two scans.

According to an embodiment of the present invention a replacement of a PDR by a polarization multiplexed LO signal solves this problem since no special absolute orientation of the polarization states SOP_H and SOP_V are required.

Other preferred embodiments are shown by the dependent claims.

It is clear that the invention can be partly embodied or supported by one or more suitable software programs, which can be stored on or otherwise provided by any kind of data carrier, and which might be executed in or by any suitable data processing unit.

BRIEF DESCRIPTION OF THE DRAWINGS

Other objects and many of the attendant advantages of the present invention will be readily appreciated and become better understood by reference to the following detailed description when considering in connection with the accompanied drawings. The components in the drawings are not necessarily to scale, emphasis instead being placed upon clearly illustrating the principles of the present invention. Features that are substantially or functionally equal or similar will be referred to with the same reference sign(s).

Fig. 1 is a schematic diagram displaying a way how to generate signals according to an embodiment of the present invention;

Fig. 2 is a graph showing two spectral components occurring in the electrical spectrum corresponding to two elements of the Jones matrix according to an embodiment of the present invention;

Fig. 3 shows a setup for multiport device characterization according to an embodiment of the present invention;

Fig. 4 shows a setup for single-scan multiport device characterization according to an embodiment of the present invention; and

Fig. 5 is a graph showing resulting spectral components when using the embodiment of Fig. 4.

DETAILED DESCRIPTION OF THE INVENTION

Embodiment of Fig. 3 shows a possible implementation of a measurement setup for multiport device characterization according to an embodiment of the present invention. A LO signal 3 coming from a tunable laser source (TLS) 4 is adjusted in its polarization to a defined polarization by a polarization setting tool 26 positioned in the path of the light beam 3 before a first beam splitter 14. The resulting incoming light beam 6 is split by the first beam splitter 14 into a first light beam 18 and a second light beam 20.

An optical device under test 2 is positioned in a first path of the first light beam 18 for coupling in the first light beam 18. A LO polarization delay unit 5 is

positioned in a second path of the second light beam 20 for coupling in the second light beam 20 for splitting the second light beam 20 into a first part and a second part, delaying the second part of the second light beam 20 relative to the first part of the second light beam 20, and recombining the first and the second part of the second light beam 20 to a resulting recombined beam 7.

A second beam splitter 28 in said first and in said second path for superimposing the first light beam 18 and the recombined beam 7 with the recombined parts of the second light beam 20 to produce interferences between the first light beam 18 and the recombined parts of the second light beam 20 in at least one resulting superimposed light beam 30 traveling a resulting path.

A detector P1 in said resulting path is then detecting the power of the resulting superimposed light beam 30 traveling the resulting path as a function of frequency and polarization when tuning the frequency of the incoming light beam 6 over a given frequency range with the TLS 4. Then, a (not shown) evaluation unit derives optical properties of the optical device under test 2 from the frequency dependency of the detected powers.

Since the PDU 5 is a multiport device the resulting beam 7 coming from the PDU 5 is distributed to four identical beam splitters 28. Accordingly, beam 18 is distributed to the four beam splitters 28. Leaving beam splitters 28 are four superimposed beams 30 which are detected by four receivers P1, P2, P3, P4 in the above described manner.

The received detector signal can be processed using the filtering setup of Fig. 1. Fig. 1 is a schematic diagram displaying a way how to generate signals according to an embodiment of the present invention. According to Fig. 3 the polarization controller 26 at the input of the system can adjust the input polarization of the PDU 5 appropriately so that the two propagation paths are excited with the same optical power. For the two-scan method according to EP 1113250, preferably two scans with orthogonal polarizations are performed. The equal power splitting inside the PDU 5 is maintained even if the input polarization is adjusted to the orthogonal state. The setup displayed in Fig. 3 has a significant reduced complexity and can be enhanced to more than four

ports without any further considerations.

Because the PDU 5 is introduced into the LO path, two orthogonal polarization states, a first state of polarization SOP_H and a second state of polarization SOP_V, occur at the output of the PDU 5. The two orthogonal components have traveled different optical paths inside the PDU 5 and thus produce interference signatures at different electrical frequencies f_H and f_V according to Fig. 2 when combined with the DUT signal 18 at the detectors P1-P4. Fig. 2 is a graph showing two spectral components occurring in the electrical spectrum corresponding to two elements of the Jones matrix

These spectral components or interference signatures created by the interference of the DUT signal 18 with signals SOP_H and SOP_V respectively can be distinguished preferably by applying band pass filters of appropriate center frequency and bandwidth.

Furthermore, amplitude and phase of the two spectral components only depend on the fraction of the DUT signal 18 having the same polarization as the interfering LO signal 7. That is, the DUT signal 18 is inherently decomposed into two polarizations SOP_H and SOP_V interfering with the corresponding two LO signals 7 and producing signatures at f_H and f_V respectively. The AC part of the detector signal can be written as follows:

$$P_{AC}(\omega) = E_{LO}E_{DUT}\left(\overrightarrow{sop}_{DUT} \cdot \overrightarrow{sop}_H\right)\cos\left(\varphi_H + \left(\underbrace{\tau_{DUT} - \tau_{LO,H}}_{f_H}\right)\omega\right) + E_{LO}E_{DUT}\left(\overrightarrow{sop}_{DUT} \cdot \overrightarrow{sop}_V\right)\cos\left(\varphi_V + \left(\underbrace{\tau_{DUT} - \tau_{LO,V}}_{f_V}\right)\omega\right)$$

To produce a signal which can be processed in the established way by the Jones matrix eigenanalysis, the two spectral components can be separated using two FIR filters according to the scheme displayed in Fig. 1. The faster oscillating signal can be shifted in frequency so that it is aligned to the slower oscillating signal. This can easily be achieved if the DGD of the PDU is known, with $DGD_{PDU} = \tau_{LO,H}-\tau_{LO,V}$. Then a linear phase term can be subtracted from the analytical signal by multiplying with $\exp(-(\tau_{LO,H}-\tau_{LO,V})\omega)$. According to Fig. 1 the

two generated signals are identical to those which would have been generated by a coherent prior art PDR detector.

The method according to this embodiment is compatible to the single-scan measurement concept described in US 09/940741, the priority of which is claimed by the present application and the disclosure of which is incorporated herein by reference.

If an additional but identical PDU 102 is inserted into the DUT path according to an embodiment of Fig. 4 showing a setup for characterizing a DUT 2 with four output ports P1-P4 using the single-scan approach, four interference signatures are generated at the receivers P1-P4. However, the DGD values of the two PDUs 5 and 102 have to be chosen appropriately to ensure that the four spectral components do not intersect. Equidistant frequency components can be generated if the two DGD values, hereafter referred to as DGD_{PDULO} and DGD_{PDUDUT}, differ by a factor of two. Furthermore, frequency components can be generated in the low-frequency range which can easily be removed by a high-pass filter.

Fig. 5. shows the resulting spectral components of the electrical spectrum. The four components J_{11}, J_{21}, J_{12}, J_{22} correspond to the four elements of the Jones matrix. They can be separated in the same way as it is done according to Fig. 1., and three of the four components J_{11}, J_{21}, J_{12}, J_{22} can be shifted in frequency to be realigned with the first component J_{11}. At this point the established Jones matrix eigenanalysis can be applied to the four signals to derive information on PMD of DUT 2.